

LESSON 27: MATRIX SOLUTION TO DIRECT STIFFNESS METHOD

- SOLUTION TO NODE DISPLACEMENTS
- SOLUTION TO MEMBER FORCES
- Matrix Inverse.

A.) NODE DISPLACEMENTS:

LAST TIME WE FOUND:

$$\bar{F}_{global} = \bar{K}_{global} \cdot \bar{\delta}_{global}$$

↑ JOINT FORCES
↑ STIFFNESS
↑ JOINT DISPLACEMENTS

BUT NOT ALL JOINTS ARE FREE TO DEFORM!
(RESTRAINTS!)

WE MUST SUBDIVIDE MATRICES:

$$\begin{bmatrix} Q_F \\ Q_S \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} \Delta_F \\ \Delta_S \end{bmatrix}$$

Q_F = JOINT FORCES AT DOF'S FREE TO DISPLACE

Q_S = JOINT FORCES AT SUPPORTED DOF'S

Δ_F = UNKNOWN JOINT DISPLACEMENTS

Δ_S = SUPPORT DISPLACEMENTS

0, unless support settlement

$$\begin{aligned} Q_F &= K_{11} \Delta_F + K_{12} \Delta_S \\ Q_S &= K_{21} \Delta_F + K_{22} \Delta_S \end{aligned}$$

UNLESS SUPPORT SETTLEMENT,
 $\Delta_S = 0$

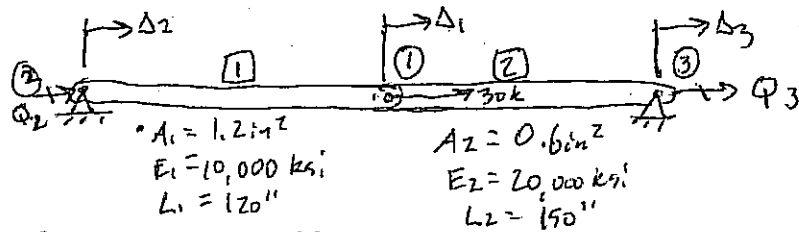
$$\left. \begin{aligned} Q_F &= K_{11} \Delta_F \\ Q_S &= K_{21} \Delta_F \end{aligned} \right\} Q_F, \quad K_{11}, K_{21} \text{ are known.}$$

Need to solve for Δ_F

$$\Delta_F = K_{11}^{-1} Q_F$$

$$Q_S = K_{21} K_{11}^{-1} Q_F \quad \leftarrow \text{FINDS SUPPORT REACTIONS}$$

NOTES: 1) Deg. of det. ? who cares! Same procedure
2) Need matrix inverse (maybe)

EXAMPLE

LOCAL STIFFNESS MATRICES

Member ①: $\bar{K}_1 = \begin{bmatrix} \text{②} & \text{①} \\ \text{①} & \text{②} \end{bmatrix} \begin{bmatrix} \frac{A_1 E_1}{L_1} & -\frac{A_1 E_1}{L_1} \\ -\frac{A_1 E_1}{L_1} & \frac{A_1 E_1}{L_1} \end{bmatrix} = \frac{1.2(10,000)}{120} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = 100 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$

MEMBER ②: $\bar{K}_2 = \begin{bmatrix} \text{①} & \text{③} \\ \text{③} & \text{①} \end{bmatrix} \begin{bmatrix} \frac{A_2 E_2}{L_2} & -\frac{A_2 E_2}{L_2} \\ -\frac{A_2 E_2}{L_2} & \frac{A_2 E_2}{L_2} \end{bmatrix} = \frac{0.6(20,000)}{150} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} = 80 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$

$$\begin{bmatrix} Q_1 \\ Q_2 \\ Q_3 \end{bmatrix} = \begin{bmatrix} \text{①} & \text{②} & \text{③} \\ 100+80 & -100 & -80 \\ -100 & 100 & 0 \\ -80 & 0 & 80 \end{bmatrix} \begin{bmatrix} \text{①} \\ \text{②} \\ \text{③} \end{bmatrix} \begin{bmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{bmatrix} \left. \begin{array}{l} \text{---} 0 \\ \text{---} 0 \end{array} \right\} \text{pinned!}$$

$$Q_f = 30 \quad K_{11} = 180 \quad K_{12} = \begin{bmatrix} -100 & -80 \end{bmatrix} \quad \Delta_f = \Delta_1$$

$$Q_s = \begin{bmatrix} Q_2 \\ Q_3 \end{bmatrix} \quad K_{21} = \begin{bmatrix} -100 \\ -80 \end{bmatrix} \quad k_{22} = \begin{bmatrix} 100 & 0 \\ 0 & 80 \end{bmatrix} \quad \Delta_s = \begin{bmatrix} \Delta_2 \\ \Delta_3 \end{bmatrix}$$

$$Q_f = K_{11} \Delta_f \rightarrow \Delta_f = K_{11}^{-1} Q_f$$

where only 1 free DOF, scalar equ.

$$\Delta_f = \left(\frac{1}{180}\right)(30) = \frac{1}{6} \text{ in}$$

SOLVE FOR REAKS:

$$Q_s = K_{21} K_{11}^{-1} Q_f$$

$$Q_s = \begin{bmatrix} -100 \\ -80 \end{bmatrix} \left[\frac{1}{180} \right] [30] = \begin{bmatrix} -100 \\ -80 \end{bmatrix} \left(\frac{1}{6} \right) = \begin{bmatrix} -16.67 \text{ k} \\ -13.33 \text{ k} \end{bmatrix}$$

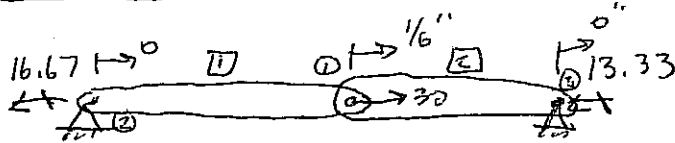
$$Q_s = \begin{bmatrix} Q_2 \\ Q_3 \end{bmatrix} = \begin{bmatrix} -16.67 \text{ k} \\ -13.33 \text{ k} \end{bmatrix}$$

B.) MEMBER FORCES

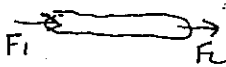
NODE ← ^{aka. joint} FORCES → MEMBER FORCES

(USE LOCAL STIFFNESS MATRIX)

PRIOR EXAMPLE:



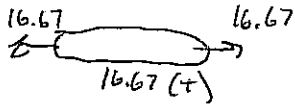
Member 1:
end forces



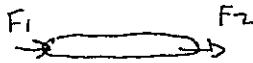
$$\begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 100 & -100 \\ -100 & 100 \end{bmatrix} \begin{bmatrix} 0 \\ 1/6 \end{bmatrix}$$

$$F_1 = -16.67 \text{ k}$$

$$F_2 = 16.67 \text{ k}$$



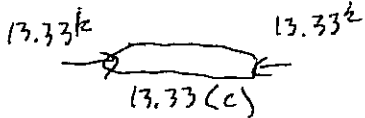
Member 2



$$\begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 80 & -80 \\ -80 & 80 \end{bmatrix} \begin{bmatrix} 1/6 \\ 0 \end{bmatrix}$$

$$F_1 = 13.33 \text{ k}$$

$$F_2 = -13.33 \text{ k}$$



C.) MATRIX INVERSE (SQUARE MATRICES ONLY)

CONSIDER 3 CASES:

(THIS COURSE IS NOT A LINEAR ALGEBRA COURSE)

CASE 1) $\bar{A} \in \mathbb{R}^{1 \times 1}$ (scalar) $\rightarrow \bar{A} = a_{11}$

$$\bar{A}^{-1} = \frac{1}{a_{11}}$$
 , matrix is a scalar, divide into 1.

CASE 2) $\bar{A} \in \mathbb{R}^{2 \times 2} \rightarrow \bar{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}$

$$\bar{A}^{-1} = \frac{\text{adj}(\bar{A})}{\det(\bar{A})} = \frac{1}{(a_{11}a_{22} - a_{12}a_{21})} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix}$$

 $\det(\bar{A}) \neq 0$

CASE 3) $\bar{A} \in \mathbb{R}^{n \times n}$

where $n > 2$

Refer to matrix algebra notes, use computational software package, etc.

(not on exam).

BONUS TOPICNUMERICAL ISSUES:

- NUMERICAL ISSUES WITH MATRIX INVERSE ARE COMMON
- A WELL PROGRAMMED SOLVER CAN OFTEN SIDESTEP THESE:

DANGEROUS APPROACH

CALCULATE K_{ii}^{-1} (many methods)
FWD $\Delta F = K_{ii}^{-1} QF$

SAFE APPROACH

DIRECT SOLN. OF:
 $\Delta F = K_{ii}^{-1} QF$
(GAUSS-JORDAN)

MAIN CAUSE OF NUMERICAL ISSUES IN STIFFNESS METHOD:

- MIXING VERY STIFF ELEMENTS w/
VERY FLEXIBLE ELEMENTS
IN GLOBAL STIFFNESS MATRIX,

 \rightarrow POSSIBLE SOLUTIONS:

- 1) IGNORE EFFECTS OF COMPLIANT MEMBERS
- 2) MULTIPLE ANALYSES